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APPENDIX I

NUCLEAR LEAVE BEHIND STUDY REPORT

Xcel Energy

Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 1 of 28

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Nuclear Leave Behind Study Report



Performed by: Craig Wrisley Jessica Kiddoo Matthew Kukacka

Transmission Planning 13 Nov, 2023 Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 2 of 28

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Table of Contents

Table of Contents

Certification
Executive Summary
Introduction10
1 Models and Assumptions11
2.1.1 Models Utilized11
2.1.2 Model Development
2.1.3 Modeling Assumption
2 Steady State Analysis
3 Stability Analysis
4 Analysis Results
5 Analysis Results Discussion
6 Observation

Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 3 of 28

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Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 4 of 28

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Certification

I hereby certify that this report was prepared by me or under my direct supervision and that I am a duly Licensed Professional Engineer under the Laws of the state of Minnesota

> Craig Wrisley 11/13/2023 License# 54948

Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 5 of 28

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Executive Summary

This analysis was performed to determine the steady state impacts and dynamic resources needed online as a result of retiring the Monticello Nuclear Generating Plant, Prairie Island Nuclear Generating Plant, and both the Monticello and Prairie Island Nuclear Generating Plants. Integrated System Planning (ISP) Transmission Planning engineers performed a study to evaluate the transmission system with the nuclear generation station retirements along with the planned Sherco coal generation replacement with Minnesota Energy Connection (MNEC) renewable generation and the AS King coal generation replacement with King Transmission Connection solar generation. Existing natural gas resources were turned on to replace the generation shortfalls based on the MISO dispatch of renewables in the model. This study is a reliability only look – system transfer capability and resource capacity analyses are out of the work scope of this study.

This study looks at the retirement of the nuclear generating stations without replacement of generation rights. The following Table M1-1 shows the retirement scenarios analyzed.

Scenario Analyzed	Monticello Generation Retired (MW)	Prairie Island Generation Retired (MW)	Total Generation Retired (MW)
Monticello Retire	637	0	637
Prairie Island Retire	0	1150	1150
Monticello and Prairie Island Retire	637	1150	1778

Table M1-1

The steady state analysis identified the retirement of the nuclear generation plants without replacement generation resulted in thermal overloads and voltage violations requiring system upgrades.

Based on the dynamic analysis results performed in this study, significant replacement generation is needed:

- Summer Peak Load Case, in addition to generation on in the base model, required all available gas generation on at Anson, Inver Grove, and Blue Lake (total 521 MW) as well as load reduction in the Twin Cities area.
 - Monticello Retire 10% (537.37 MW)
 - \circ Prairie Island Retire 20% (1074.74 MW)
 - Monticello and Prairie Island Retire 30% (1612.11 MW)
- Shoulder Load Average Wind Case, in addition to the generation on in the base model required additional combustion generation turned on.
 - Monticello Retire High Bridge 7 and 9 (388MW), Riverside 7 and 9 (318 MW). Total generation addition of 706 MW.
 - Prairie Island Retire High Bridge 7 and 9 (388MW), Riverside 7, 9, and 10 (476 MW), Blue Lake 7 and 8 (302 MW). Total generation addition of 1,166 MW.

Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 6 of 28

PUBLIC DOCUMENT—NOT-PUBLIC DATA HAS BEEN EXCISED INCLUDES TRADE SECRET AND CEII DATA YELLOW HIGHLIGHT DENOTES PROTECTED DATA

Monticello and Prairie Island Retire – High Bridge 7, 8, and 9 (550 MW), Riverside 7, 9, and 10 (476 MW), Blue Lake 1-4, 7, and 8 (455MW), Inver Grove 1-6 (282 MW). Total generation addition of 1763 MW.

Scenarios Analyzed

2028 Summer Shoulder Average Wind, and Summer Peak scenarios are analyzed in this study. Renewables in the NSP system are modeled at seasonal generation levels; Solar at 50% for Summer Peak, 31% for Summer Shoulder Average Wind, Wind at 15.5% for Summer Peak, 27% for Summer Shoulder Average Wind.

NSP load information is shown in following Table M1-2.

NSP Load Level						
Year	Season	Load Level				
2028	Summer Shoulder Average Wind	6,383 MW				
2028	Summer Peak	9,064 MW				

Table M1-2

Steady State Simulation Results

Steady state analysis was performed on the base case, Monticello retire case, Prairie Island retire case, and both Monticello and Prairie Island retire case for both the Summer Peak and Summer Shoulder Average Wind case. Available NSP natural gas generation was turned on to reduce the number of unsolved contingencies. The number of unique facilities with new or increased >0.5% voltage violations and thermal violations beyond the preexisting violations in the base case and associated costs to mitigate them for each case are listed in Table M1-3.

 Table M1-3

 Voltage and Thermal Upgrades with cost for Steady State Violations

Transient Stability Simulation Results

Transient stability analysis was performed on the base case, Monticello retire case, Prairie Island retire case, and both Monticello and Prairie Island retire case for both the Summer Peak and

Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 7 of 28

PUBLIC DOCUMENT—NOT-PUBLIC DATA HAS BEEN EXCISED INCLUDES TRADE SECRET AND CEII DATA YELLOW HIGHLIGHT DENOTES PROTECTED DATA

Summer Shoulder Average Wind case. Available NSP natural gas generation was turned on to achieve stable dynamic response. If no additional NSP natural gas resources were available, load in the Twin Cities area was scaled down to achieve stable dynamic response.

Uti.	Generation and Loud Mujustments with cost for Stable Dynamic Response									
	S	Summer Peak		Sum	ummer Shoulder					
Scenario Analyzed	Additional Generation On (MW/\$)	Load Reduction (MW/\$)	Total Cost (\$)	Additional Generation On (MW)	Load Reduction (MW)	Total Cost (\$)				

 Table M1-4

 Generation and Load Adjustments with cost for Stable Dynamic Response

Without Twin Cities Load reduction for the summer peak case, and additional gas generation turned on in both summer peak and shoulder average wind case, generator rotor angles exceed +/- 300 degrees, which is indicative of the point where the generator would lose synchronization with the grid and trip offline. Example plots of Unstable and Stable Response are shown in Figure M1-1 and Figure M1-2.

Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 8 of 28

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Figure M1-1 2028SHAW Unstable Generator Angle Response



Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 9 of 28

PUBLIC DOCUMENT—NOT-PUBLIC DATA HAS BEEN EXCISED INCLUDES TRADE SECRET AND CEII DATA YELLOW HIGHLIGHT DENOTES PROTECTED DATA

The second of t		Euc # 248796 248899 248893 251849	But Name 07MBROMI 22 07WORTHI 13. G064_07L_WI 1	.0HL .8 8 13.8	MAN	LAK But 3 3 3
SHAW2028_Monti_off with MNEC and ASKtr ANS MEC HBR7_9 RVS7_MISO23_2028_SHA	₩_ • •	Bus # 248796 248893 251849	Bus Name 07MEROM1 22 07WORTH1 13. G084_07LAW11	.0HL .8 8 13.8	ID 1 1	LAK But 3 3 3
Generator relative angle (deg) : Reference Generator = 200034 [PCHBTM 2 22.0]* 1* 70 42 42 14 14	0 • •	But # 248796 248899 248893 251849	But Name 07MEROM1 22. 07WORTH1 13. G084_07LAW11	.8 8 13.8	10 1 1	But. 3 3
Generator relative angle (deg) : Reference Generator = 200034 [PCHBTM 2 22.0]* 1*	0 • •	Buc # 248796 248899 248893 251849	Buc Name 07MEROM1 22. 07WORTH1 13. G084_07LAW1 10.	.8 8 13.8	1D 1 1 1	But. 3 3
Benerator relative angle (deg) : Reference Generator = 200034 [PCHBTM 2 22.0]* 1* 70 42 42 14 14	0 • •	Bus # 248796 248899 248893 251849	Bus Name 07MEROM1 22 07WORTH1 13. G084_07LAW1 1	.8 8 13.8	10 1 1 1	Buf. 3 3
Benerator relative angle (deg) : Reference Generator = 200034 [PCHBTM 2 22.0]* 1* 70 42 42 14 14 14	0 • •	But # 248796 248889 248893 251849	Вик Name 07MEROM1 22. 07WORTH1 13. G084_07LAW11	.8 8 13.8	1 1 1	But. 3 3
	0 • • 0	248796 248889 248893 251849	07MEROMI 22. 07WORTHI 13. G084_07LAWI 1	.8 8 13.8	1 1 1	3
	⊕ □	248893 251849	G084_07LAW1 1	a 13.8	1	3
	ŏ	251849	0004_07LAWI1	13.6	1	
	19	101040			1	3
		251861	08GIB1 24.0		î.	1
		251878	08VERML1 13.8	8	i	3
	X	251899	08WHTLD3 13	8	3	-
	1	251901	G43108EDWCT1	18.0	G1	3
	Δ	251952	08MADSN1 13.	8	1	3
	V	253502	10J089_CULG21	4.4	2	3
	Ŧ	253506	10ABB_G1 22.0)	1	3
	Ψ	253594	10WAR_G4 20.	0	4	3
	\diamond	253625	10G849_CANG1	6.90	1	3
	+	253763	10SAB_G1 13.2		1	3
	•	254813	PETERSBURG 32	22.0	3	3
		254801	GEORGETOWN	113.8	1G	3
	B	254827	16EVCT1 17.1		1	3
	•	254847	STOUT 7 22.0		7	3
		255232	17SCHAFER-172	4.0	17	3
	⊞	255236	17MI_CITY-1222	.0	12	3
	•	255240	17WCE-GT1 18.	0	1	3
0.00 6.00 12.00 18.00 24.00 30.00	Δ	255441	17SGR_CK-CTAI	18.0	G1	3
Time (sec)	v	255496	17STJ1(J351)18.0		1	3

Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 10 of 28

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Introduction

This analysis was performed to determine the steady state impacts and dynamic resources needed online as a result of separately retiring the Monticello Nuclear Generating Plant and the Prairie Island Nuclear Generating Plant. For further analysis, the retirements of both the Monticello and Prairie Island Nuclear Generating Plants simultaneously were included in the analysis. Additionally, Integrated System Planning (ISP) Transmission Planning engineers performed a study to evaluate the transmission system steady state with the nuclear generation station retirements along with the planned Sherco coal generation replacement with Minnesota Energy Connection (MNEC) renewable generation. Existing natural gas resources were turned on to replace the generation shortfalls based on the MISO dispatch of renewables in the model. This study is a reliability only look – system transfer capability and resource capacity analyses are out of the work scope of this study.

Assumptions

This study is performed utilizing Siemens PSSE version 35.3.2 for steady state analysis and Powertech TSAT version 22.3.39 for dynamic analysis and based on the MISO Transmission Expansion Plan (MTEP) 2023 steady state models and dynamics package. MISO MTEP 2023 series, year 2028 models are selected as the starting models; no substantial load growth is assumed in this study. Sherco coal generation is replaced with Minnesota Energy Connection renewable generation at MISO renewable dispatch levels. AS King coal generation is replaced with King Transmission Connection solar generation at MISO solar dispatch levels.

Potential Limitations

Model

Sherco and King generation replacement locations and details are assumed based on the preliminary project scope, final project details may have minor differences.

Retirement of the nuclear generating stations were assumed to have no replacement generation installed. Load reduction where needed for stability was performed as a percent reduction across all loads in the Twin Cities area.

Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 11 of 28

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1 Models and Assumptions

1.1.1 Models Utilized

Siemens PSSE version 35.3.2 for steady state analysis and Powertech TSAT version 22.3.39 for dynamic analysis and based on the MISO MTEP 2023 steady state models and dynamics package. MISO MTEP 2023 series, year 2028 models are selected as the starting models; no substantial load growth is assumed in this study.

1.1.2 Model Development

MTEP 2023, year 2028 Summer Peak (SUM) and 2028 Shoulder Average Wind (SHAW) models are selected as the starting models. Sherco coal generation is replaced with Minnesota Energy Connection renewable generation at MISO renewable dispatch levels. AS King coal generation is replaced with King Transmission Connection solar generation at MISO solar dispatch levels.

2028 Summer Shoulder Average Wind, and Summer Peak scenarios are analyzed in this study. Renewables in the NSP system are modeled at seasonal generation levels; Solar at 50% for Summer Peak and 31% for Summer Shoulder Average Wind; Wind at 15.5% for Summer Peak and 27% for Summer Shoulder Average Wind. NSP load information is shown in Table M1-5.

NSP	NSP Load Level and Thermal Generation Level					
Year	Season	Load Level				
2028	Summer Shoulder Average Wind	6,383 MW				
2028	Summer Peak	9,064 MW				

 Table M1-5

 NSP Load Level and Thermal Generation Level

1.1.3 Modeling Assumption

MTEP 2023, year 2028 Summer Peak (SUM) and 2028 Shoulder Average Wind (SHAW) models are selected as the starting models. Sherco coal generation is replaced with Minnesota Energy Connection renewable generation at MISO renewable dispatch levels. AS King coal generation is replaced with King Transmission Connection solar generation at MISO solar dispatch levels. Analysis is performed on cases with Monticello Nuclear Generating Plant retired, Prairie Island Nuclear Generating Plant retired, and both Monticello and Prairie Island Nuclear Generating Plants retired.

Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 12 of 28

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2 Steady State Analysis

Xcel Energy

MISO MTEP 2023 Steady State 2033SUM and 2033SHAW models are used to conduct the steady state analysis. Steady analysis was performed on the base case, Monticello retire case, Prairie Island retire case, and both Monticello and Prairie Island retire case for both the Summer Peak and Summer Shoulder Average Wind case. Full N-1 and N-1-1 contingencies were run for LRZ 1.

Available NSP natural gas generation was turned on to reduce the number of unsolved contingencies. Robust solution in PSSE was used to allow for system adjustment of reactive devices and generation during contingency analysis to reduce the number of unsolved contingencies.

3 Stability Analysis

MISO MTEP 2023 Transient Dynamic package is used to conduct the transient stability analysis. Three phase faults with normal clearance time and single line to ground faults with a stuck breaker are tested for major 345 kV substations, transmission lines in Twin Cities and neighboring areas. Selected 345 kV bus voltages and transmission line power flow in Twin Cities and neighboring areas are monitored and plotted. The disturbances studied are listed in Table M1-6:

YELLOW HIGHLIGHT DENOTES PROTECTED CEII DATA

Name	Description
0693 redacted	·
0857 redacted	
0860 redacted	
0865 redacted	
0866 redacted	
0867 redacted	
0868 redacted	
0879 redacted	
0890 redacted	
0891 redacted	
0892 redacted	
0893 redacted	
0896 redacted	
0898 redacted	
0920 redacted	
0922 redacted	
0927	

Table M1-6

Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 13 of 28

PUBLIC DOCUMENT—NOT-PUBLIC DATA HAS BEEN EXCISED INCLUDES TRADE SECRET AND CEII DATA YELLOW HIGHLIGHT DENOTES PROTECTED DATA

Name	Description
0935 redacted	
0936 redacted	
0941 redacted	
0942 redacted	
0943 redacted	
0944 redacted	
0945 redacted	
2199 redacted	
2218 redacted	
2219 redacted	
2229 redacted	
2238 redacted	
2242 redacted	
2257 redacted	
2277 redacted	

PROTECTED CEII DATA ENDS

Available natural gas generation was turned on iteratively to achieve stability. Where insufficient natural gas generation was available to achieve stability, scalable load in the Twin Cities was reduced by a percentage of area load until stability was achieved.

- Summer Peak Load Case, in addition to generation on in the base model, required all available generation on at Anson, Inver Grove, and Blue Lake (total 521 MW) as well as load reduction in the Twin Cities area.
 - Monticello Retire 10% (537.37 MW)
 - Prairie Island Retire 20% (1,074.74 MW)
 - Monticello and Prairie Island Retire 30% (1,612.11 MW)
- Shoulder Load Average Wind Case, in addition to the generation on in the base model required additional combustion generation turned on.
 - Monticello Retire High Bridge 7 and 9 (388 MW), River Side 7 and 9 (318 MW). Total generation addition of 706 MW.
 - Prairie Island Retire High Bridge 7 and 9 (388 MW), River Side 7, 9, and 10 (476 MW), Blue Lake 7 and 8 (302 MW). Total generation addition of 1,166 MW.
 - Monticello and Prairie Island Retire High Bridge 7, 8, and 9 (550 MW), Riverside 7, 9, and 10 (476 MW), Blue Lake 1-4, 7, and 8 (455 MW), Inver Grove 1-6 (282 MW). Total generation addition of 1,763 MW.

4 Analysis Results

In the steady state analysis, available NSP natural gas generation was turned on to reduce the number of unsolved contingencies. The number of unique facilities with new or increased >0.5% voltage violations and thermal violations beyond preexisting violations in the base case were

Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 14 of 28

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identified. Associated costs assigned based on MISO Transmission Cost Estimation Guide For MTEP23¹ for rebuild of overloaded lines to larger conductor size and assuming 5 150MVAR statcoms, situated in the vicinity of the retired nuclear units would resolve the voltage violations observed. The cost breakdown of the associated upgrades is listed in Table M1-7:

v uita	ge and ther	mai upgi au	es with cost i	of Steauy St	ale violation	15

 Table M1-7

 Voltage and Thermal Upgrades with cost for Steady State Violations

In the dynamic analysis, available NSP natural gas generation was iteratively turned on to achieve stability. Once all available NSP natural gas was turned on, Twin Cities load was scaled down to achieve stability. Generation additions and load reduction are summarized in Table M1-8:

	Summe	er Peak	Summer Shoulder		
Scenario Analyzed	Additional Generation On (MW)	Load Reduction (MW)	Additional Generation On (MW)	Load Reduction (MW)	
Monticello Retire	512	537.37	706	0	
Prairie Island Retire	512	1074.74	1,166	0	
Monticello and Prairie Island Retire	512	1612.11	1,763	0	

 Table M1-8

 Generation and Load Adjustments for Stable Dynamic Response

¹ MISO Transmission Cost Estimation Guide for MTEP23337433.pdf (misoenergy.org)

Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 15 of 28

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5 Analysis Results Discussion

For the steady state results, any line with thermal violations is assumed to need an upgrade. Transformers with thermal violations are assumed to be replaced with transformer sized to carry the contingency level flows. Voltage violations are assumed to need reactive support in the form of capacitors or reactors. MISO cost estimation values are used to determine the estimated cost of upgrades as summarized in Table M1-9.

		Summer Peak		S	ummer Shoulder	
	Line Upgrade (miles/cost \$)	Reactive Support (MVAR/cost \$)	Total Cost (\$)	Line Upgrade (miles/cost \$)	Reactive Support (MVAR/cost \$)	Total Cost (\$)
Monticello Retire						
Prairie Island Retire						
Monticello and Prairie Island Retire						

Table M1-9Steady State Upgrade Summary

For the dynamic results, cost was applied to the natural gas units turned on to maintain system stability assuming gas price of [redacted]. Cost was also applied to load reduction to maintain system stability in the Summer Peak load case. Costs associated with dynamic stability are summarized in Table M1-10.

 Table M1-10

 Dynamic Generation and Load Adjustments Costs

	S	Summer Peak	Sum	ummer Shoulder				
Scenario Analyzed	Additional Generation On (MW/\$)	Load Reduction (MW/\$)	Total Cost (\$)	Additional Generation On (MW)	Load Reduction (MW)	Total Cost (\$)		
Monticello								
Retire								
Prairie								
Island								
Retire								
Monticello								
and Prairie								
Island								
Retire								

Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 16 of 28

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2028 Summer Peak Case:

Generator angular stability issues were identified at generation and load reduction levels below those indicated in Table 6 as indicated by generator angles exceeding +/- 300 degrees, which reflects the angle at which the generator would lose synchronization with the electric grid and trip offline. Indicative plot of angular instability is shown in Figure M1-3. Stable generator angle plot examples for each retirement scenario are shown in Figure M1-4, Figure M1-5, and Figure M1-6.



Figure M1-3 SUM28 Prairie Island and Monticello Retirement Angular Instability

Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 17 of 28

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Figure M1-4 SUM28 Monticello Retirement Angular Stability



Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 18 of 28

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Figure M1-5 SUM28 Prairie Island Retirement Angular Stability



Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 19 of 28

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Figure M1-6 SUM28 Prairie Island and Monticello Retirement Angular Stability



Bus Voltage and Frequency were also montiored with no identified instability.

2028 Summer Shoulder Average Wind Case:

Generator angular stability issues were identified at generation levels below those indicated in Table 6 as indicated by generator angles exceeding +/- 300 degrees, which reflects the angle at which the generator would lose synchronization with the electric grid and trip offline. Indicative plot of angular instability is shown in Figure M1-7. Stable generator angle plot examples for each retirement scenario are shown in Figure M1-8, Figure M1-9, and Figure M1-10.

Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 20 of 28

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Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 21 of 28

PUBLIC DOCUMENT—NOT-PUBLIC DATA HAS BEEN EXCISED INCLUDES TRADE SECRET AND CEII DATA YELLOW HIGHLIGHT DENOTES PROTECTED DATA

Figure M1-8 SHAW28 Monticello Retirement Angular Stability



Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 22 of 28

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Figure M1-9		
SHAW28 Prairie Island Retirement An	gular Stability	
Buf. Binary Recult File Scenario	Contingency	
2 SHAW2028_PI_off with MNEC and ASKtc ANS MEC HBR7_9 RVS7_9_10 E:MISO23_2028_S	3HAW_1 0693_W_GRE_P42_KOH	ILMAN_L#
Generator relative angle (dee) - References Generator = 20004 (PCHRTM 2 - 22.01* 4*	But # But Name	ID Buf.
	O 248796 07MEROM1 22.8	1 2
	248889 07WORTH1 13.8	1 2
	248893 G084_07LAW1 13.8	1 2
	251849 08CAY1 18.0	1 2
42 0 0 0 0	251861 08GIB1 24.0	1 2
	251878 08VERML1 13.8	1 2
	△ 251899 08WHTLD3 13.8	3 2
	▲ 251901 G43108EDWCT118.0	G1 2
14	▲ 251952 08MADSN1 13.8	1 2
		2 2
	253506 10ABB_G1 22.0	1 2
	↓ 253594 10WAR_G4 20.0	4 2
	♦ 253625 10G849_CANG16.90	1 2
	253763 10SAB_G1 13.2	1 2
	254813 PETERSBURG 322.0	3 2
	254801 GEORGETOWN 113.8	1G 2
	254827 16EVCT1 17.1	1 2
	254847 STOUT 7 22.0	7 2
	255232 17SCHAFER-1724.0	17 2
	E 255236 17MI_CITY-1222.0	12 2
	▲ 255240 17WCE-GT1 18.0	1 2
0.00 6.00 12.00 18.00 24.00 30.00	▲ 255441 17SGR_CK-CTA18.0	G1 2
Time (sec)	▼ 255496 17STJ1(J351)18.0	1 2

Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 23 of 28

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Bus Voltage and Frequency were also montiored with no identified instability.

Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 24 of 28

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6 Observation

Xcel Energy

Based on the steady state results performed in this study, significant line upgrades and voltages support are needed to mitigate violations with their associated fixed costs as a result of the retirement of the nuclear units:

		Summer Peak				Summer Shoulder		
	Line Upgrade (miles/cost \$)	Reactive Support (MVAR/cost \$)	Total (\$)	Cost	Line Upgrade (miles/cost \$)	Reactive Support (MVAR/cost \$)	Total (\$)	Cost
Monticello Retire								
Prairie Island Retire								
Monticello and Prairie Island Retire								

 Table M1-11

 Steady State Upgrade Cost Summary

Based on the dynamic analysis results performed in this study, significant replacement generation is needed along with the associated annual costs of the generation:

- Summer Peak Load Case, added generation to achieve generator angular stability needed was 521 MW as well as load reduction in the Twin Cities area based on the nuclear generation being retired.
 - Monticello Retire 10% (537.37 MW) Total Annual Cost [redacted].
 - Prairie Island Retire 20% (1,074.74 MW) Total Annual Cost [redacted].
 - Monticello and Prairie Island Retire 30% (1,612.11 MW) Total Annual Cost [redacted]
- Shoulder Load Average Wind Case, added generation to achieve generation angular stability based on the nuclear generation being retired.
 - Monticello Retire Total generation addition of 706 MW Total Annual Cost [redacted]
 - Prairie Island Retire Total generation addition of 1,166 MW Total Annual Cost [redacted]
 - Monticello and Prairie Island Retire Total generation addition of 1,763 MW Total Annual Cost [redated]

Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 25 of 28

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PUBLIC DOCUMENT—NOT-PUBLIC DATA HAS BEEN EXCISED INCLUDES TRADE SECRET AND CEII DATA YELLOW HIGHLIGHT DENOTES PROTECTED DATA

Appendix 1 – Steady State Analysis Thermal Overloads

YELLOW HIGHLIGHT DENOTES PROTECTED CEIL DATA

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Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 26 of 28

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Page 26

Xcel Energy

Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 27 of 28

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Page 27

Docket No. E002/RP-24-67 Appendix M1: Nuclear Leave Behind Study Report - Page 28 of 28

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Nuclear Leave Behind Study

PROTECTED CEII DATA ENDS